(1) for Figures NB-3643.3(a)-1, sketches (a) and (b):

\[ t_n = \frac{n}{b} L_1 \geq 0.5 \left( \frac{d_m n}{b} \right)^{1/2} \]

\[ t_n = T_b' \text{ if } L_1 < 0.5 \left( \frac{d_m n}{b} \right)^{1/2} \]

(2) for Figure NB-3643.3(a)-1, sketch (c):

\[ t_n = T_b' + \left( \frac{2}{3} \right) \nu \text{ if } \theta \leq 30 \text{ deg} \]

\[ t_n = T_b' + 0.385 L_1 \text{ if } \theta > 30 \text{ deg} \]

(3) for Figure NB-3643.3(a)-1, sketch (d):

\[ t_n = T_b' = T_b \]

(d) Peak Stress Indices. The peak stress indices \( K_{2b} \) and \( K_{2r} \), for moment loadings [see NB-3683.1(d)] shall be taken as:

\( K_{2b} = 2.0 \)

\( K_{2r} = 1.6 \)

(e) For branch connections made with fillet or partial penetration welds per NB-3661.3, the stress indices given in Table NB-3681(a)-1 and in NB-3683.8 shall be increased as follows:

1. The \( B \) and \( B \) indices shall be increased by a factor of 1.5.
2. \( C_{2b} \) and \( C_{2r} \) shall be multiplied by 2.
3. \( K_{1}, K_{2b}, \) and \( K_{3} \) shall be multiplied by 3.
4. \( K_{2b} \) shall be multiplied by 2.
5. \( C_{2b} \) shall be a minimum of 6.0.
6. \( C_{2r} \) shall be a minimum of 4.2.

In calculating the indices for fillet and partial penetration welded branch connections, \( T_{2b} \) may be taken to be \( t_n \), with the other dimensions consistent with Figure NB-3643.3(a)-1.

NB-3683.9 Butt Welding Tees. The stress indices given in Table NB-3681(a)-1, except as modified herein and in NB-3683.2, are applicable to butt welding tees manufactured to the requirements of ASME B16.9 or MSS SP-87.

(a) Primary Stress Indices. The primary stress indices \( B_{2b} \) and \( B_{2r} \) shall be taken as:

\[ B_{2b} = 0.4 \left( \frac{R_m}{T} \right)^{1/2} \text{ but not } < 1.0 \]

\[ B_{2r} = 0.50 \left( \frac{R_m}{T} \right)^{1/3} \text{ but not } < 1.0 \]